ROCHESTER INSTITUTE OF TEHNOLOGY MICROELECTRONIC ENGINEERING

# Microelectromechanical Systems (MEMs) Unit Processes for MEMs Deposition

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## **OUTLINE**

Oxide Growth Diffusion Physical Vapor Deposition LPCVD Epitaxy Spin Coating Lift-Off Copper Plating Wafer Bonding Anodic Bonding

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### **OXIDE GROWTH CALCULATOR**





## **OXIDE THICKNESS COLOR CHART**

Thick ness	Color
500	Tan
700	Brown
1000	Dark Violet - Red Violet
1200	Royal Blue Blue
1500	Light Blue - Metallic Blue
1700	Metallic - very light Yellow Green
2000	LIght Gold or Yellow - Slightly Metallic
2200	Gold with slight Yellow Orange
2500	Orange - Melon
2700	Red Violet
3000	Blue - Violet Blue
3100	Blue Blue
3200	Blue - Blue Green
3400	Light Green
3500	Green - Yellow Green
3600	Yellow Green
3700	Yellow
3900	Light Orange
4100	Carnation Pink
4200	Violet Red
4400	Red Violet
4600	Violet
4700	Blue Violet

Thickness	Color
4900	Eile Blue
5000	Blue Green
5200	Green
5400	Yellow Green
5600	GreenYellow
5700	Yellow -"Yellowish" (at times appears to be Lt gray or matel
5800	Light Orange or Yellow - Pink
60 00	Carnation Pink
6300	Violet Red
6800	"Buish" (appears violet red, Blue Green, looks Blue
7200	Blue Green - Green
7700	"Yellowish"
80 00	Orange
8200	Salmon
8500	Dull, Light Red Violet
8600	Violet
8700	Blue Violet
8900	Blue
9200	Blue Green
9500	Dull Yellow Green
9700	Yellow - "Yellowish"
9900	Orange
10000	Carnation Pink



Nitride Thickness = (Oxide Thickness)(Oxide Index/Nitride Index) Eg. Yellow Nitride Thickness = (2000)(1.46/2.00) = 1460



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	MEM	ls Depositio	n	
DIFFU	SION MA	SKING	CAL	CULATOR
Select				
Boron or Phosp	horous		R	ay Krom, 2007
Enter				·
Temperature an	d Time			
Rochester Institute of	of Technology			Raymond Krom
Microelectronic Engi	neering			Dr. Lynn Fuller
9.5.07				Raymond Krom
Diffusion Mask Calcul	ator	Enter 1-Yes	0-No in	white boxes
		Temperature	s must b	e between 1000C and 1200C
Dement	Diffusion		or result v	will be in error.
Boron	Diffusion	1100	°C	
Phosphorous 1	Time	100	minutes	
,			Boron	1867 Angstroms
Oxide			Phosp	6399 Angstroms
Fitted to data taken fr	om Hamilton and	Howard		6399 Angstroms
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DIFFUS	SION CON SOL	ISTANTS UBILITY	AND SO	LID
	<u></u>	UBLIY		
DIFF	USION CONSTA	NTS		
BORON	PHOSPHOROUS	PHOSPHOROUS	BORON	PHOSPHOROUS
DRIVE-IN	PRE	DRIVE-IN	SOLID	SOLID
			SOLUBILITY	SOLUBILITY
			NOB	NOP
1.07E-15 cm2/s	2.09e-14 cm2/s	7.49E-16 cm2/s	4.75E20 cm-3	6.75E20 cm-3
4.32E-15	6.11E-14	3.29E-15	4.65E20	7.97E20
1.57E-14	1.65E-13	1.28E-14	4.825E20	9.200E20
5.15E-14	4.11E-13	4.52E-14	5.000E20	1.043E21
1.55E-13	9.61E-13	1.46E-13	5.175E20	1.165E21
4.34E-13	2.12E-12	4.31E-13	5.350E20	1.288E21
1.13E-12	4.42E-12	1.19E-12	5.525E20	1.410E21
2.76E-12	8.78E-12	3.65E-12	5.700E20	1.533E21
			PLAVR	ACK NEVI
Rochester Institu Microelectronic F	te of Technology Engineering			
	© Santambar 19 2	12 Dr. Lynn Fullar Brof		
	DIFF BORON DRIVE-IN 1.07E-15 cm2/s 4.32E-15 1.57E-14 5.15E-14 1.55E-13 4.34E-13 1.13E-12 2.76E-12	DIFFUSION CONSTAT         BORON       PHOSPHOROUS         DRIVE-IN       PRE         1.07E-15 cm2/s       2.09e-14 cm2/s         4.32E-15       6.11E-14         1.57E-14       1.65E-13         5.15E-14       4.11E-13         1.55E-13       9.61E-13         4.34E-13       2.12E-12         1.13E-12       4.42E-12         2.76E-12       8.78E-12	DIFFUSION CONSTANTS           BORON         PHOSPHOROUS         PHOSPHOROUS           DRIVE-IN         PRE         DRIVE-IN           1.07E-15 cm2/s         2.09e-14 cm2/s         7.49E-16 cm2/s           4.32E-15         6.11E-14         3.29E-15           1.57E-14         1.65E-13         1.28E-14           5.15E-14         4.11E-13         4.52E-14           1.55E-13         9.61E-13         1.46E-13           4.34E-13         2.12E-12         4.31E-13           1.13E-12         4.42E-12         1.19E-12           2.76E-12         8.78E-12         3.65E-12	DIFFUSION CONSTAUTS         BORON DRIVE-IN       PHOSPHOROUS PRE       PHOSPHOROUS DRIVE-IN       BORON SOLUB         107IC-15 cm2/s       2.09e-14 cm2/s       7.49E-16 cm2/s       4.75E20 cm-3         4.32E-15       6.11E-14       3.29E-15       4.65E20         1.57E-14       1.65E-13       1.28E-14       4.825E20         5.15E-14       4.11E-13       4.52E-14       5.000E20         1.55E-13       9.61E-13       1.46E-13       5.175E20         4.34E-13       2.12E-12       4.31E-13       5.350E20         1.13E-12       4.42E-12       1.19E-12       5.525E20         2.76E-12       8.78E-12       3.65E-12       5.700E20





# **DIFFUSION AND DRIVE IN CALCULATIONS**

Starting w aler kesistivity		Rho =	<u> </u>	
Starting W afer Type		n-type = 1	1 1 or 0	
		p-type = 1	0 1 or 0	
Pre Deposition Temperature			950 °C	
Pre Deposition Time			<u>15</u> min	
Drive-in Temperature			1100 °C	
Drive-in Time		I	480 min	
CALCULATE			<u>VALUE</u> UNITS	
Solid Solubility at Temperature of Pre Deposition	1		4.65E+20 cm-3	
Diffusion Constant at Temperature of Pre Depos	ition		3.93E-15 cm/sec	
Diffusion Constant at Temperature of Drive-in		l	1.43E-13 cm/sec	
CALCULATION OF DIFFUSION CONSTANTS	5			
	D0 (cm2/s)	EA (eV)		
Boron	0.76	3.46		
Phosphorous	3.85	3.66		
NOB = 3.5E17 (T) + 1.325E20				
NOP = 2.45E18(T) - 1.53E21				
CALCULATIONS			VALUE UNITS	
Substrate Doping = $1/(q \mu max Rho)$			4.42E+14 cm-3	
Ratio of Nsub/Ns =			9.51E-07	
Approximate inverse erfc from $erfc(u) = e^{-u^2} / (u(t))$	oi)^0.5)		3.47	
RESULTS			VALUE UNITS	
xi after pre deposition = $((4Dp tp)^{05})^{*}(inv erfc)$	Nsub/Ns))		0.13 um	
Pre deposition Dose. $OA = 2N_0 (Dr tr/\pi)^{-0.5}$			9.87E+14 atoms /cm2	
xi after drive-in = ((4 Dd td/OA) ln (Nsub ( $\pi$ Ddtd	0^0.5))^0.5		4.03 um	
average doping Nave = $Dose/xj$			2.45E+18 atoms /c m3	
mobility ( $\mu$ ) at Doping equal to Nave			109 cm2/V-s	
Sheet Desisten as $= 1/(q (u(Nava)))Daga)$			58 ohms	
Sheet Resistance = $I/(q (\mu(Nave)))Dose)$			01110	

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### **DIFFUSION FROM A LIMITED SOURCE**



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## **EXAMPLE**

1. A predeposit from a p-type spin-on dopant into a 1E15 cm-3 wafer is done at 1100°C for 10 min. Calculate the resulting junction depth and dose.

# **SOLUTION**

2. The spin-on dopant is removed and the Boron is driven in for 2 hours at 1100 °C. What is the new junction depth?

**SOLUTION** 







# **DIFFUSION EXAMPLE**

**Example:** Single crystal silicon can be selectively etched. Regions with dopant concentration greater than 1e19 etch much slower than lighter doped regions. Design a process to create a 2 micrometer diaphragm.



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# **DOPING POLYSILICON**

When using poly as a conductor in integrated circuits it is desirable to have low resistivity. Doping at 1000 °C for 20 min using Emulsitone Co., 19 Leslie Court, Whippany, NJ 07981 Tel (201)386-0053; Emitter Diffusion Source N250 spin-on dopant gives 10-15 ohm/sq sheet resistance for 0.75 um thick poly. (The Allied Signal Inc., 1090 South Milpitas Boulevard, Milpitas, CA 95035, Tel (408)946-2411, Accuspin P-854 dopant gives higher resistivity in the range of 100 ohm/sq.)

2 um Poly Doped n+ using N-250 for 30 min  $@ 1100 \text{ C} \qquad \text{rhos} = 8 \text{ ohms}$   $@ 950 \text{ C} \qquad \text{rhos} = 40 \text{ ohms}$   $@ 800 \text{ C} \qquad \text{rhos} = 10,000 \text{ ohms}$ 

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## **ION IMPLANT**

### See separate lecture notes on ion implant.

### **Important results are:**

depth (range) vs energy spread (straggle) vs energy gaussian implant profile equation  $N(x)=\{Dose/(2\pi \Delta Rp^2)^{-0.5}\}EXP^{-[(x-Rp^2)/2\Delta Rp^2]}$ Dose = It/qArea masking for selective implantation sheet resistance (ohms) = 1/ (qµDose) MOSFET threshold voltage adjust = +/- qDose/Cox'

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# VACUUM PUMPS, GAUGES AND SYSTEMS

See separate lecture notes on Backend Wafer Processing (back\_end.ppt) Pages 6-34



Rotary Vane Mechanical Pump



Ion pump



Magnetically levitated turbomolecular pumps on HDPCVD system

Not shown: Diffusion Pump Cryo Pump Sublimation Pump Penning Gage





### **EVAPORATION CALCULATION**

Notice     Nation 19, 2000       Microelectronic Engineering     Dr. Lynn Fuller       Exaporation in this model assumes that the mass exeporated is spread out over the inside surface.       of a sphere with radius equal to the distance from the evaporation source to the substrate. The surface area is 4 p if when multiplied by film thickness gives volume of material needed which is multiplied by the density to give the mass needed. Dude the mass by 2 if a dimplet bat is used allowing coating over a hemisphere instead of a sphere.       m = the mass that needs to be evaporated = 4 p ih <sup>2</sup> f c     m = 3.88 gm       f = the density of the material being evaporated     d = 19.3       h = the height between the filament and the substrate     h = 40 cm       mass in truy oz is found = 0.3215 x mass (g)     m = 0.12 Troy Oz       Aluminum 2.7     0       Gold     19.3       I = the denial     Select only one =1, others = 0       Aluminum 2.7     0       Gold     19.3       I = the denial     Select only one =1, others = 0       Aluminum 2.7     0       Gold     19.3       I = the denial     Select only one =1, others = 0       Aluminum 2.7     0       Gold     19.3       I = the denial     Select only one =1, others = 0		Pachastar batituta of Tachaolas	N	More	b 10 2006		
Indexection Englisering       Differential         Evaporation in this model assumes that the mass evaporated is spread out over the inside surface of a sphere with radus equal to the distance from the evaporation source to the substrate. The surface area is 4 pi h <sup>2</sup> when multiplied by film thickness gives volume of material needed which is multiplied by the density to give the mass needed. Divide the mass by 2 if a dimpled boat is used allowing coating over a hemisphere instead of a sphere.         m = the mass that needs to be evaporated       4 pi h <sup>2</sup> f c       m = 3.88 gm         f = the desined film thickness       f = 0.1 µm         d = the density of the material being evaporated       d = 19.3         h = the height between the filament and the substrate       h = 40 cm         mass in troy oz is found = 0.3215 x mass (p)       m = 0.12 Troy Oz         Deristy of some materials       Select only one =1, others = 0         Aluminum       2.7       0         Gold       19.3       1         Copper       8.98       0         Tin       7.3       0         Lead       11.4       0         Dimed Boat       1       1	-	Microelectropic Engineering			l vnn Fuller		
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d = the density of the material being evaporated     d = 19.3       h = the height between the filament and the substrate     h = 40 cm       mass in troy oz is found = 0.3215 x mass (g)     m = 0.12 Troy Oz       Denisty of some materials     Select only one =1, others = 0       Aluminum     2.7     0       Gold     19.3       Tin     7.3     0       Lead     11.4     0	-	f = the desired film thickness		f =	0.1 µ	um	
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Substrate f $hf = \frac{m}{4d \pi h^2}f = film thickness$	-				Dillipled Bo	<u>al</u>	
$f = \frac{m}{4d \pi h^2}$	-	A	Substrate	1000			
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$f = \frac{m}{4d \pi h^2}$	-						
f = film thickness	•		$f = \frac{m}{44\pi h^2}$				
Current f = film thickness			+d π n*				
		Comment V	f = film thickness				
d = density	┼┶╫╲		d = density				
h = hcieht	TET Roche		h = hcight				
Micro	Micro	ෂා	m = mass				
		_	111 111035				
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# **EVAPORATION TECHNIQUES**

**Aluminum** - evaporate copper with tungsten wire basket. One pellet at 20 cm gives about 3000 A.

**Copper -** evaporate copper with tungsten wire basket. The basket needs to be crushed a little so the openings are small and the copper does not fall out of the basket once it is melted. One pellet at 20 cm gives about 3000 A. Dimpled Tungsten boats work great.

**Chromium** – use special Chromium coated tungsten wire filaments. Current through the filament heats the Cr which sublimes.

**Gold** - gold or gold/germanium can easily be evaporated from a basket with tightly spaced loops. The basket needs to be crushed a little so the openings are small and the gold does not fall out of the basket once it is melted. Dimpled

Tantalum boats work great.

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## **CHROME EVAPORATION**

Deposit chrome by evaporation (actually sublimation) from special chrome coated tungsten rods. Using the CVC evaporator. Heat rods to red hot by setting filament voltage to 190 on the dial. Then open the shutter for the desired time calculated from rate of 35 Å/sec. (at a distance of 40 cm from source to substrate)



R.D.Mathis P.O. Box 92916 Long Beach, CA 90809-2916 <u>www.rdmathis.com</u>

Part No. ?? Cost \$250/50 qty

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### **DEPOSITION OF SILICON MONOXIDE (SiO)**

Evaporate SiO with Ta boat and cover with hole. The material sublimes and a film will be deposited. It looks like glass and can be measured on the ellipsometer. The ellipsometer gave an index of refraction of 1.88

Using the CVC evaporator X mg at 40 cm gives about 300 Å. Set to 250 on the dial.

R.D.Mathis P.O. Box 92916 Long Beach, CA 90809-2916 <u>www.rdmathis.com</u>

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Part No. Cost





		MEMs Depositio	n		
	EVA	<b>PORATIO</b> N	DATA		
Material Formula	Melt pt.	Temp °C @	Vapor Pressui	e 1E (	16.4
		Ĵ	1E-8	1E-0	1E-4
Aluminum	Al	660	677	812	1010
Alumina	Al2O3	2045	1045	1210	1325
Antimony	Sb	630	279	345	425
Arsenic	As	814	107	152	210
Beryllium	Be	1278	710	878	1000
Boron	B	2100	1278	1548	1797
Cadmium	Cd	321	64	120	180
<b>Cadmium Sulfide</b>	CdS	1750			550
Chromium	Cr	1890	837	977	1177
Cobalt	Со	1495	850	990	1200
Gallium	Ga	30	619	742	907
Germanium	Ge	937	812	957	1167

MRC Co., "Evaporation and Sputtering Data Book," Orangeburg, NY http://www.epimbe.com/pages/vp

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## **EVAPORATION DATA**

Material Formula Melt pt.

Temp °C @ Vapor Pressure

	_		°C	_	1E-8	1E-6	1E-4
Gold	Au		1062		807	947	1132
Hafnium Oxide	HfO2		2812				2500
Nickel	Ni		1453		927	<b>987</b>	1262
Palladium	Pd		1550		842	<b>992</b>	1192
Platinum	Pt		1769		1292	1492	1747
Selenium	Se		217		<b>89</b>	125	170
Silicon	Si		1410		<b>992</b>	1147	1337
Silicon Dioxide	SiO2		1800				1025
Silicon Nitride	Si3N4						800
Silver	Ag		961		574	617	684
Tantalum	Ta		2966		1960	2240	2590
Titanium Ti		1668		1067	1235	1453	
<b>Tungsten W</b>		3410		2117	2407	2757	
Zirconium	Zr		1852		1477	1702	<b>1987</b>

MRC Co., "Evaporation and Sputtering Data Book," Orangeburg, NY http://www.epimbe.com/pages/vp

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# **SPUTTERING**

**DC Sputtering** - Sputtering can be achieved by applying large (~2000) DC voltages to the target (cathode). A plasma discharge will be established and the Ar+ ions will be attracted to and impact the target sputtering off target atoms. In DC sputtering the target must be electrically conductive otherwise the target surface will charge up with the collection of Ar+ ions and repel other argon ions, halting the process.

**RF Sputtering** - Radio Frequency (RF) sputtering will allow the sputtering of targets that are electrical insulators (SiO2, etc). The target attracts Argon ions during one half of the cycle and electrons during the other half cycle. The electrons are more mobile and build up a negative charge called self bias that aids in attracting the Argon ions which does the sputtering.



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### **SPUTTERING**

**Magnetron Sputtering** - Magnets buried in the baseplate under the target material cause the argon ions and electrons to concentrate in certain regions near the surface of the target. This increases the sputtering rate.



### **SPUTTER TARGETS**

### PE 2400 Targets

Au Ta2O5 Zr Cr SiO2 Qty2 Qty2 Ta Si Mg TiO2 NiFe Nb2O5 CrSiO In2O5 Qty2 Nb Permalloy SnO2 Fe A12O3 AlNi MgF2 NiFeMg MgO Ni Target Insulators 3 Co **Backing Plates6** 

### **2" Unbonded for Denton** Gold Palladium



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#### **SPUTTER TARGETS**

#### 8" Bonded for CVC-601

Aluminum 100% Aluminum/1% Silicon Chrome Chrome Oxide Copper Molybdenum Tantalum Titanium Titanium10%/Tungsten 90% Silicon Dioxide Silicon Indium Tin Oxide **8''Unbonded for CVC-601** Molybdenum/Titanium Titanium/Al 1%/Silicon 2%

#### 4" Unbonded for CVC 601

Chrome Indium 90%/Tin 10% Nickel Tantalum Tin Nickel-Chromium 80%/20% 108E-6 ohm cm, TCR 110 E-6/°C \$450- 4"x1/4" Mel Hollander, Research and PVD Materials Corp. (973) 575-4245

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## **RIT SPUTTERING DATA**

Material	Head	Power (watts)	Rate
Aluminum	8"	2000	240 Å/min.
Nickel	4"	500	170
Chromium	8"	1350	350
InSn + O2	4"	100	80
Copper	8"	325	110
Gold*	2"	40 mA,50mTorr	250
Tantalum	4"	500	190
Titanium	8"	1350	220
Tungsten	4"	500	100
Tungsten	8"	1000	115
Palladium#	2"	10mA, 90 mTorr	100

This data is for the CVC 601 Sputter System at 5 mTorr Argon Pressure, Base Pressure Prior to Sputter <1E-5 \*Denton Sputter Machine

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#### **STRESS IN SPUTTERED FILMS**

Compressively stressed films would like to expand parallel to the substrate surface, and in the extreme, films in compressive stress will buckle up on the substrate. Films in tensile stress, on the other hand, would like to contract parallel to the substrate, and may crack if their elastic limits are exceeded. In general stresses in films range from 1E8 to 5E10 dynes/cm2.



## STRESS IN SPUTTERED TUNGSTEN FILMS

#### Tungsten

CVC 601 4" Target 500 Watts 50 minutes 5 mTorr Argon Thickness ~ 0.8 μm



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Picture from scanner in gowning

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## **REACTIVE SPUTTERING**

**Reactive Sputtering -** introducing gases such as oxygen and nitrogen during sputtering can result in the deposition of films such as indium tin oxide (ITO) or titanium nitride TiN (other examples include AlN,  $Al_2O_3$ , AnO  $Ta_2O_5$ )

**Unwanted Background Gases in Sputtering -** Most Films are very reactive when deposited. Water and oxygen cause rougher films, poorer step coverage, discoloration (brown aluminum), poorer electrical properties, etc.







MEMs Deposition		
CVD CHEMISTRY		
Epi	$SiCl4 + 2H2 \longrightarrow Si + 4HCl$	
Polysilicon	SiH4 (gas) → Si (solid) + 2H2	
Silicon Nitride	SiCl2 H2 + NH4 $\longrightarrow$ Si3N4 + HCl	
Low Temperature Oxide	$SiH4 + O2 \longrightarrow SiO2 + H2$	
Tungsten (Selective on Si not on SiO2)	WF6 + 3H2 $\longrightarrow$ W + 6HF	
TEOS (tetraethyl orthosilicate)	$Si(C2H5O)4 \longrightarrow SiO2 + 4C2H4 + 2 H2O$	
TiN (TDMAT) reduction of Ti[N(CH2CH3)2]4		
Copper CVD	reduction of ???	
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# **MEMs Deposition RIT LPCVD TOOLS** 4" LPCVD 6" LPCVD Top Tube for LTO Bottom Tube for Poly and Nitride

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## **LTO**

Wafers are loaded back to back in caged boat. The boat is filled with dummy wafer to total 25 wafers. Monitor wafer is placed in the middle.



#### Caged Boat

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#### **PECVD OXIDE FROM TEOS**

TEOS Program: (Chamber A) Step 1 Setup Time = 15 secPressure = 9 TorrSusceptor Temperature= 390 C Susceptor Spacing= 220 mils RF Power = 0 watts TEOS Flow = 400 sccO2 Flow = 285 sccStep 2 – Deposition  $\hat{\text{Dep Time}} = 55 \text{ sec } (5000 \text{ Å})$ Pressure = 9 TorrSusceptor Temperature= 390 C Susceptor Spacing= 220 mils RF Power = 205 watts TEOS Flow = 400 sccO2 Flow = 285 sccStep 3 – Clean Time =  $10 \sec$ Pressure = Fully Open Susceptor Temperature= 390 C Susceptor Spacing= 999 mils RF Power = 50 watts TEOS Flow = 0 sccO2 Flow = 285 scc



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#### **STRESS IN POLY AND NITRIDE FILMS**



Stress in poly films can cause buckling and bending of beams and cantilever structures. When doping poly after deposition the high temperatures (1000 C) anneal stress. Undoped poly structures require an anneal.



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## **STRESS IN NITRIDE FILMS**

Stress in an 8000 A Nitride Film causing fracture



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MEMs Deposition LOW STRESS SILICON RICH Si3N4 ADE Measured stress for various Dichlorosilane: Ammonia Flow Ratios Flow Stress x E 9 dynes/cm2 10:1 +14.63 5:1 +14.81 2.5:1 +12.47 Stress;  $\sigma = (E/(6(1-v)))*(D^2/(rt))$ 1:1 +10.13 where E is Youngs modulus, 1:2.5 +7.79\* v is Poissons ratio, 1:5 +3 D and t are substrate and film thickness 1:10 r is radius of curvature (+ for tensile)  $\mathbf{O}$ \*standard recipe T.H Wu, "Stress in PSG and Nitride Films as Related to Film Properties and Annealing", Solid State Technology, p 65-71, May '92  $10 \text{ dyne/cm}^2 = 1 \text{ newton/m}^2 = 1 \text{ Pascal}$ **Rochester Institute of Technology** Microelectronic Engineering

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MEMs Deposition **MEASUREMENT OF STRESS IN Si3N4** Kenneth L. Way, Jr. did his senior project on stress in silicon nitride films as a function of the ratio of ammonia to dichlorosilane. Samples were coated with various flows and stress was measured at ADE corporation. The silicon nitride was etched off of the backside of the wafer so that the stress curvature was due to the layer on the front side only. Dr. Lane said the nitride runs at 1:10 (ammonia:dichlorosilane) ratios are rough on the pumping system. **Compressive Stress Tensile Stress** Dr. Grande sent samples to Kodak for stress measurement. He found stress of +900 MPa Tensile for the standard Nitride recipe for 1500 A thickness, 1-29-2000 **Rochester Institute of Technology** Microelectronic Engineering  $10 \text{ dyne/cm}^2 = 1 \text{ newton/m}^2 = 1 \text{ Pascal}$ © September 18, 2012 Dr. Lynn Fuller, Professor Page 54



## NITRIDE THICKNESS COLOR CHART

-	<u>Thickness</u>	Color
	200	Silver
	400	Brown
	550	Yellow-brown
	730	Red Violet
	770	Deep Blue
	930	Blue
	1000	Pale Blue
	1100	Very Pale Blue
	1200	Silver
	1300	Light Yellow
	1500	Yellow
	1800	Orangfe-Red
L	1900	Red Violet
	2100	Dark Red
	2300	Blue
	2500	Blue-Green
L	2800	Light Green
L	3000	Orange-Yellow
	3300	Red Violet
L		
Rocheste		
Microele		

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## **APPLY PARYLENE**

Approximately 1 gm of Parylene C gives ~3000Å film thickness, Deposit 5 wafers per run.

#### Adhesion Promotor

(gammamethacryloxypropyltrimethoxysilane) spin coat 3000 rpm 1 min. Bake 110 C for 2 min. Then load into Parylene Deposition Tool.





See: http://www.scscookson.com/parylene/properties.cfm

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## PECVD OF CARBON FILM (DIAMOND LIKE FILM)

Drytech Quad Tool CH4 flow 45 sccm 50 mTorr 200 Watt Deposition Rate ~ 320 Å/min Index of Refraction = 2.0





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## LPCVD

The placement of the wafers in the boat and the placement of the boat in the furnace and the temperature of the furnace all affect the deposition rate. Rates from 35 A/min to 100 A/min have been observed with basically the same LPCVD recipe. 80 A/min was obtained by simply spacing the dummy wafers and the device wafers in every other slot in the boat. Starting in the 5th slot place 5 dummy wafers in every other slot followed by 5 device wafers and two dummies all spaced every other slot. Place the boat such that the 1st device wafer is slightly closer to the door so that all device wafers are forward with respect to the center of the furnace. 5 or 10 degrees hotter will also give a higher deposition rate. For thick layers do the deposition in two runs and switch the order to give more uniform deposition. Flats up and all wafers pretty much vertical also helps uniformity. These films are not as dense as thermal oxide. They etch faster in BHF and KOH etches.







## **POLYIMIDE**

Polyimide has a melting point of 450 C, can be spin coated and imaged with lithographic processes making it useful for many applications.

Using DuPont Corporations PI-2555 we can get film thickness between 2.5  $\mu$ m @ 5000 rpm and 5.0  $\mu$ m @ 1500 rpm. It is cured by placing on 120 °C hot plate for 30 min. and then on a 350 °C hot plate for 30 min. Multilayer coatings can give thickness greater than 10  $\mu$ m. (a 500 gm bottle costs ~\$250) Du Pont Co., Electronic Materials Division, Barley Mill Plaza, Reynolds Mill Building, Wilmington, DE 19898 (800)441-7543

OCG Microelectronic Materials, Belgium, makes a polyimide "Proimide 114A" which we have used.

These film are easily imaged using an aluminum barrier layer and conventional photoresist (such as Shipley System-8) followed by Oxygen Reactive Ion Etch.



## **COPPER PLATING**

Mix about 65g of Copper Sulfate (CuSO<sub>4</sub>) crystals to 200 ml of water plus water. Make sure there are no undissolved solids in the mixture. When done, the solution should look dark blue. To increase the conductivity of the solution, add about 5 ml of Sulfuric acid using a pipette.

Wet the O-ring to make a better seal.

Set the DC voltage supply to get a current density of about 3 mA/cm2. (15 mA for 1 inch diameter circular area of exposed copper) Plate copper for about 45 min.

$$CuSO_4 + H_2O => Cu^{2+} + SO^{2-}_4 + H_2O$$



## **COPPER PLATING**

Copper Sulfate (CuSO<sub>4</sub>) + water- CuSO<sub>4</sub> + $H_2O =>Cu^{2+}+SO^{2-}_4+H_2O$ 

When a voltage is applied and a current flows, the copper ions  $(Cu^{2+})$  will move towards the negative electrode (cathode), where it gains an electron and becomes a copper molecule (2Cu). At the same time the sulfate ion  $(SO^{2-}_4)$  will be attracted to the anode where it becomes a sulfate molecule.

Adhesion and uniformity of the plating is a function of the rate of deposition and the substrate material. It was found that Cu will not plate on aluminum or chrome but will plate on nickel but nickel will not stick to aluminum so the following film stack was used to plate onto silicon (for solder bump contacts). Plated Copper (2 to 10  $\mu$ m) on evaporated Copper (2500 A) on Nickel (2400 A) on Chrome (1000 A) on Aluminum (7000 A) on Silicon.

## **COPPER PLATING APPARATUS**



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## **GOLD PLATING**

Electroless gold solution can be used on copper or nickel films. This chemically replace copper atoms with gold atoms. Can only plate up to the original copper film thickness. Immerse copper in heated 80 C gold plating bath for 10 min.

Electroplating of gold is also common.



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#### **EVALUATION OF FILM PROPERTIES**

Thickness Stress Morphology Stociometery Grain Size Contact Angle More



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## SEM OF FILM MORPHOLOGY



Polysilicon Substrate

6-7-99

Rochester Institute of Technology Microelectronic Engineering Polymer Film on Poly



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## WAFER BONDING

Silicon Direct: No Voltage, Temp 800 to 1100 C, No Intermediate Layer, Very Clean Surface, Very Flat Surface

Anodic (Glass to Silicon): Voltage 300 to 2000, Temp 300 to 500 C, No Intermediate Layer, Special Glass Required (7740)

Sputtered Pyrex: Voltage 20 to 200, Temp 300 to 500, Layer 1 to 5 µm

**Thermal Oxide:** Voltage 10 to 30, Temp 1100 C, Layer 1 to 3 µm

Spin On Glass: No Voltage, Temp 200 to 500 C, Layer 30 to 100 nm, borosilicate or phosphoro/borosilicate spin on glass.

Eutectic: No Voltage, Temp just below Eutectic Point, Scrubbing Action and Pressure Needed,

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# DIRECT Si-Si FUSION BONDING

Direct fusion bonding - two wafers with or without SiO2 can be directly bonded by placing them together and heating to 800 C and followed by anneal at temperatures up to 1100 C in oxygen or nitrogen. The two surfaces can be hydrophilic or hydrophobic. (The RCA clean makes the surface of bare silicon wafers hydrophilic. An HF dip makes the surface hydrophobic.)

See Karl Suss tools for wafer bonding www.suss.com



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### **SURFACE PREPARATION**

RCA clean followed by 10 min HF gives contact angle of 52°, Hydrophobic Surface

RCA clean gives contact angle of 4.5°, Hydrophilic Surface



Contact angle measurement of a water drop on a silicon surface

(A) RCA clean NH<sub>4</sub>OH:H<sub>2</sub>O<sub>2</sub>:H<sub>2</sub>O = 1:1:6 for 10 min at 75 °C, HCl:H<sub>2</sub>O<sub>2</sub>:H<sub>2</sub>O = 1:1:6 for 10 min at 75 °C,
(B) H<sub>2</sub>O:H<sub>2</sub>O<sub>2</sub>:NH<sub>4</sub>OH = 6:1:4 for 10 min at 55 °C
(C) RCA clean and 65% HNO<sub>3</sub> for 10 min
(D) RCA clean and 2% HF for 10 min

- (E)  $H_2SO_4$ :  $H_2O_2 = 5:1$  for 10 min
- (F) 30% H2SO4 for 10 min

At the end of the pretreatments the wafers were always rinsed in deionized water.

pretreatment	direct after pretreatment	5 h	27 h	3 d	6 J
A	4.5°	5.5*	9°	16°	20°
В	5.5°	4°	5.5°	7.5°	12*
С	1°	4°	4°	12.5°	16.5
D	52°	61°	63.5°	59.5°	57"
E	1.5°	4°	6°	17°	22°
F	51°	46°	45°	.47.5°	45°

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## WAFER BONDING RESULTS



Shiny surfaces against each other,

- 1100 C in Furnace14
- time = 30 minutes
- dry O2 (5 lpm)



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# **ANODIC BONDING**

Anodic bonding is used to permanently bond a glass sheet to a silicon wafer at low temperature (~400C) using a combination of heat and high electric field.











# FUEL INJECTOR PROJECT









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### **MEMs Deposition** WET OXIDE GROWTH CHART EXAMPLE 1 10 6000Å -X<sub>ox</sub>,(um) 201 **10**<sup>-1</sup> 24 <del>60</del> 900 10<sup>-2</sup> 100 10 1,000 t, Time, (min) Rochester Institute of Technology **50 min** Microelectronic Engineering © September 18, 2012 Dr. Lynn Fuller, Professor Page 84





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