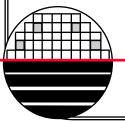
# ROCHESTER INSTITUTE OF TECHNOLOGY MICROELECTRONIC ENGINEERING

# **MEM Switches**

# Dr. Lynn Fuller, Artur Nigmatulin, Andrew Estroff

Microelectronic Engineering
Rochester Institute of Technology
82 Lomb Memorial Drive
Rochester, NY 14623-5604
Tel (585) 475-2035
Fax (585) 475-5041
Lynn.Fuller@rit.edu
http://people.rit.edu/lffeee





Rochester Institute of Technology

### ADOBE PRESENTER

This PowerPoint module has been published using Adobe Presenter. Please click on the Notes tab in the left panel to read the instructors comments for each slide. Manually advance the slide by clicking on the play arrow or pressing the page down key.



### **OUTLINE**

Introduction

**Applications** 

General Purpose Relays

**RF** Switches

**Electrostatic Actuation** 

Magnetic Actuation

**Patents** 



Rochester Institute of Technology

### **INTRODUCTION**

Excellent Isolation >40dB@10Ghz

Low Loss <1dB@2Ghz

Low On Resistance < 1 ohm

High Q > 10,000

Low Power Consumption (almost zero)

High Currents ~1 Amp and 10 Amp Peak

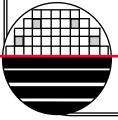
Small Size

Low Actuation Voltage <6 Volts

Reliability >10E9 Cycles

Fast Operation 10-100 µsec

Small Packaging



Rochester Institute of Technology

# **APPLICATIONS**

Area	System	Device
	Communication and	Switch
Phased Array	Radar Systems	(ground , space, airborne, missile)
	Wireless	
	Communication	
	(portable, base station)	
Switching and	switches	Switch
Reconfigurable	Satellite	
Networks	(Communication and	
	Radar)	
	Airborne	
	(Communication and	
	Radar)	
Low power	Wireless	
oscillators	Satellite	Varactors and inductors
and amplifiers	Airborne	

### CANTILEVER TYPE SWITCH

Drain Source

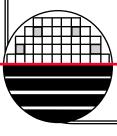
$$F = \frac{\epsilon_o \epsilon_r A V^2}{2d^2}$$

Gold

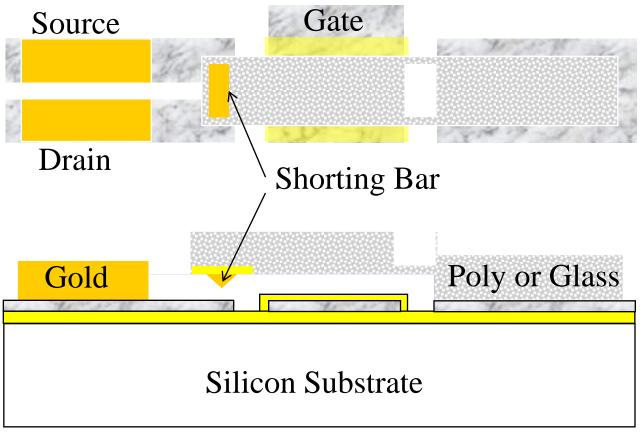
Gold

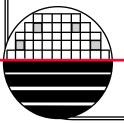
Silicon Substrate





### CANTILEVER TYPE SWITCH – SHORTING BAR





$$F = \frac{\varepsilon_0 \varepsilon_r A V^2}{2d^2}$$

### ADI MEMS SWITCH

Size 100 μm x 100 μm

Contacts Gate

Drain

Sour

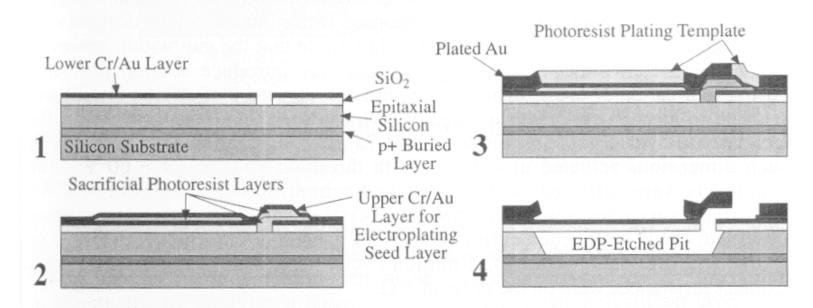
Deflection

Figure 1. ADI MEMS Switch Configuration

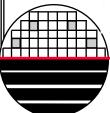


Rochester Institute of Technology

### SINGLE CONTACT SWITCH



Cross-sectional diagrams of a single-contact micromechanical switch at various stages during the fabrication procedure. (1) After first metal etch and oxide etch. (2) After evaporation of Au-Cr plating base. (3) After selective Au plating through photoresist plating template. (4) Finished structure after photoresist stripping, removal of excess plating base, and EDP etch. After Petersen (1978a).



### PACKAGED SWITCH

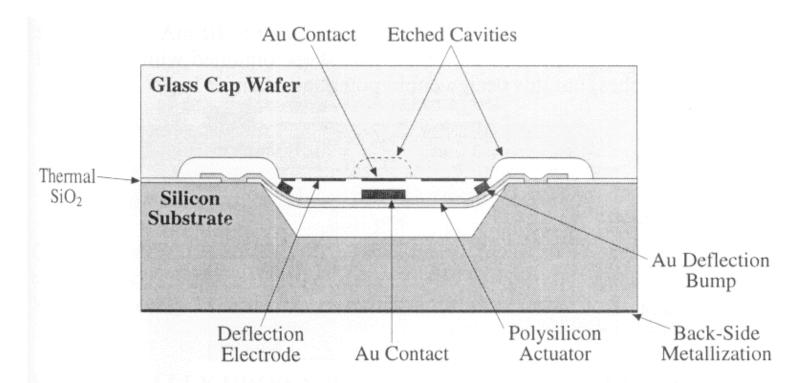
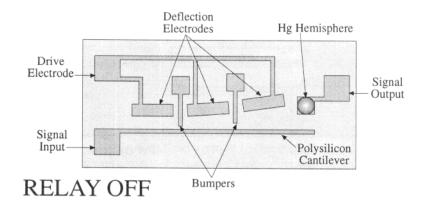
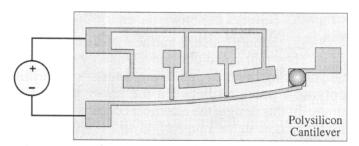


Illustration of a bulk micromachined, electrostatically actuated relay. Adapted from Drake, et al. (1995).

Rochester Institute of Technology

# LATERAL MOVEMENT, Hg CONTACT SWITCH

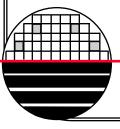




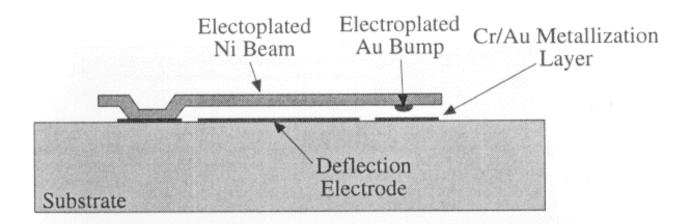
### **RELAY ON**

Illustration of a surface micromachined, mercury-contact electrostatic relay in the off state (top) and on state (bottom). Adapted from Saffer, et al. (1995).

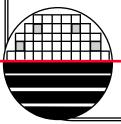
Rochester Institute of Technology



### ALL METAL SWITCH



Cross-sectional illustration of a surface micromachined, electrostatic relay, fabricated by electroplating Au bump contacts and Ni beams above a sacrificial copper layer (not shown). Adapted from Zavracky, et al. (1997).



Rochester Institute of Technology

### **MAGNETIC RELAY**

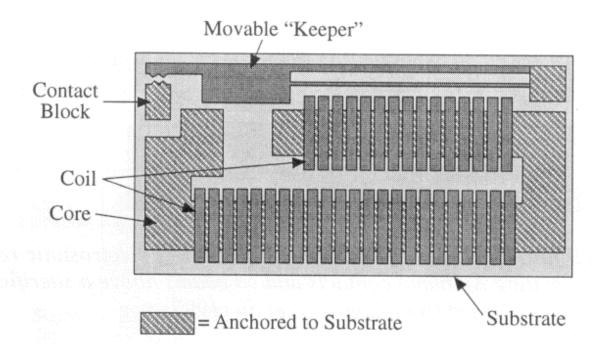


Illustration of monolithic, micromachined magnetic relay. Adapted from Rogge, et al. (1995).



Rochester Institute of Technology

### MAGNETIC LATCHING RF SWITCH

### **Operation Principle**

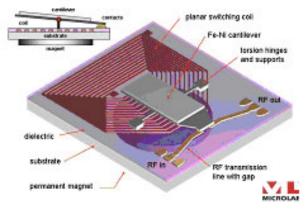
# www.magfusion.com

The principle behind the latching characteristics is the preferential magnetization of a cantilever made of soft magnetic material (e.g. permalloy). In a constant, nearly perpendicular magnetic field, a cantilever can have either a clockwise or a counter-clockwise torque depending on the angle between the cantilever and the field, which leads to the bistability. To change state of the switch, a second magnetic field (generated by a short current pulse through a coil in this case) realigns the magnetization of the cantilever and changes the direction of the magnetic torque, causing the cantilever to flip. The static external magnetic field instantly latches the switch in the closed or open position. The switch maintains this state until the next switching signal realigns the cantilever magnetization. The relay consumes no power to maintain the latched state.

### MagLatch™ RF Switch

The superior performance figures demonstrated by the product prototypes have positioned Magfusion to introduce several high performance products in areas such as wireless communications, portable RF devices, consumer and industrial electronics, aerospace, automotive electronics, and automatic testing equipment. The switch operates with short (< 100  $\mu$ s) current pulses and low control voltage (< 5 V).

### MagLatch™ RF MEMS Switch

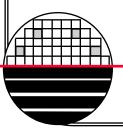




### MAGNETIC LATCHING RF SWITCH

### **Benefits**

- Bi-stable, power supply is not required to hold the states, no power in quiescent states
- Operation voltage < 5 V, below 2 V demonstrated</li>
- Switching energy < 50 mJ, switching current < 100 mA, switching time < 100 ms</li>
- Provides low insertion loss, high isolation, high linearity
- High reliability (billions of cycles demonstrated)
- Operation in ambient environment (potentially lower packaging cost)
- Conventional microelectronic fabrication technology may be employed, reducing production costs
- Can be fabricated on a variety of substrates: Si, GaAs, glass, metal, ceramic, magnets, etc.
   Capable of post Si IC process and integration
- Small dimension ( $\sim$  1 mm  $\times$  2 mm per SPDT relay, much smaller dimension [0.1 mm  $\times$  0.1 mm] have been demonstrated)
- SPST, MPST, or MPDT capable. Non-latching type is available upon customer request.



www.magfusion.com

### CAPACITIVELY COUPLED RF SWITCH

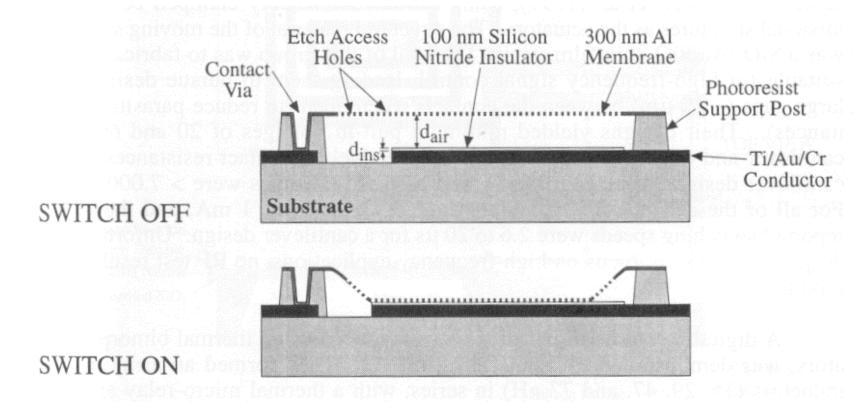
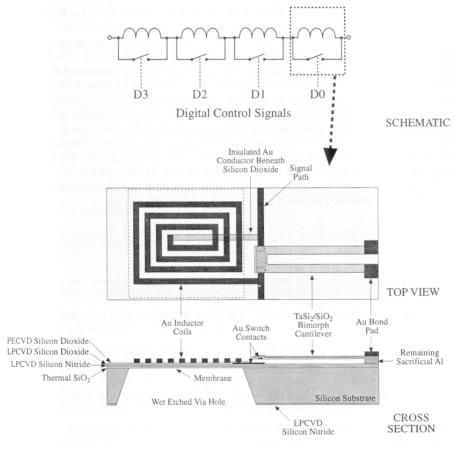
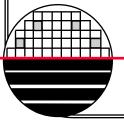


Illustration of a capacitively coupled, electrostatically actuated membrane-type RF switch. Adapted from Goldsmith, et al. (1996).

### INDUCTOR ARRAY WITH THERMAL BIMORPH SWITCHES





Rochester 1 Microelecti Illustration of a micromachined, digitally controlled inductor array, using thermal bimorph actuators for switching. Adapted from Zhou, et al. (1997). As seen in the schematic (top), one of the series inductor/switch combinations are shown in the top view (center) and cross section (bottom). When a particular switch is actuated, it bypasses the associated inductor.

6,069,540

May 30, 2000

### **PATENTS**



### United States Patent [19]

Berenz et al.

[54] MICRO-ELECTRO SYSTEM (MEMS) SWITCH

[75] Inventors: John J. Berenz, San Pedro; George W. McIver, Redondo Beach; Alfred E. Lee, Torrance, all of Calif.

Assignee: TRW Inc., Redondo Reach, Calif.

[21] Appl. No.: 09/418,341 [22] Filed: Oct. 14, 1999

### Related U.S. Application Data

Continuation of application No. 08/897,075, Apr. 23, 1999, abandoned.

Int. Cl.7 ..... ...... H01P 1/10; H01H 57/00 

Field of Search ..... .... 333/101, 105-107, 333/262; 200/181, 339

### [56] References Cited

### U.S. PATENT DOCUMENTS

4,203,017 5/1980 Lee ... 5,638,946 6/1997 Zavracky

### FOREIGN PATENT DOCUMENTS

08235997 9/1996 Japan

Primary Examiner-Paul Gensler Attorney, Agent, or Firm-Michael S. Yatsko

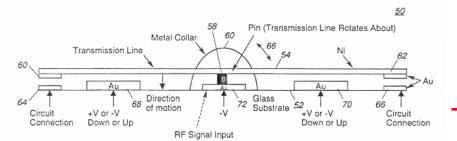
Patent Number:

Date of Patent:

### ABSTRACT

An RF switch formed as a micro electro-mechanical switch (MEMS) which can be configured in an array forming a micro electro-mechanical switch array (MEMSA). The MEMS is formed on a substrate. A pin, pivotally carried by the substrate defines a pivot point. A rigid beam or transmission line is generally centrally disposed on the pin forming a teeter-totter configuration. The use of a rigid beam and the configuration eliminates the torsional and bending forces of the beam which can reduce reliability. The switch is adapted to be monolithically integrated with other monolithic microwave integrated circuits (MMIC) for example from HBTs and HEMTs, by separating such MMICs from the switch by way of a suitable polymer layer, such as polyimide, enabling the switch to be monolithically integrated with other circuitry. In order to reduce insertion losses, the beam is formed from all metal, which improves the sensitivity of the switch and also allows the switch to be used in RF switching applications. By forming the beam from all metal, the switch will have lower insertion loss than other switches which use SiO2 or mix metal contacts.

### 22 Claims, 14 Drawing Sheets



### United States Patent [19]

Loo et al.

[54] DESIGN AND FABRICATION OF BROADBAND SURFACE-MICROMACHINED MICRO-ELECTRO-MECHANICAL SWITCHES FOR MICROWAVE AND MILLIMETER-WAVE APPLICATIONS

[75] Inventors: Robert Y. Loo, Agoura Hills; Adele Schmitz, Newbury; Julia Brown, Santa Monica; Jonathan Lynch, Oxnard; Debabani Choudhury, Woodland Hills; James Foschaar, Thousand Oaks, all of Calif.: Daniel J. Hyman, Cleveland Hts., Ohio; Brett Warneke, Berkeley, Calif.; Juan Lam, Agoura Hills, Calif.; Tsung-Yuan Hsu, Westlake Village, Calif.; Jae Lee, University Heights; Mehran Mehregany, Pepper Pike, both of Ohio

[73] Assignees: Hughes Electronics Corporation, El Segundo, Calif.; Rosemont Aerospace, Inc., Burnsville, Minn.

[21] Appl. No.: 09/080,326

May 15, 1998 [22] Filed:

[51] Int. Cl.7 ..... H01P 1/10; H01H 57/00 333/262; 200/181; 200/600 U.S. Cl. .... ...... 333/262; 200/181,

[58] Field of Search ......

Patent Number:

6,046,659

Date of Patent:

Apr. 4, 2000

### [56] References Cited

### U.S. PATENT DOCUMENTS

5,578,976		Yao 333/262	
5,629,565		Schlaak et al 200/181 X	
5,638,946	6/1997	Zavracky 200/181	

### FOREIGN PATENT DOCUMENTS

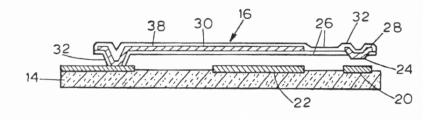
63-54801 3/1988 Japan ...... 333/262

Primary Examiner-Justin P. Bettendorf Attorney, Agent, or Firm-V. D. Duraiswamy; M. W. Sales

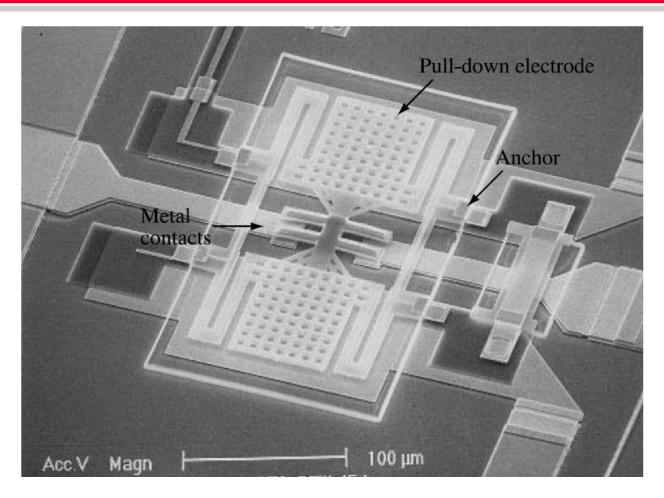
### ABSTRACT

Methods for the design and fabrication of micro-electromechanical switches are disclosed. Two different switch designs with three different switch fabrication techniques are presented for a total of six switch structures. Each switch has a multiple-layer armature with a suspended biasing electrode and a conducting transmission line affixed to the structural layer of the armature. A conducting dimple is connected to the conducting line to provide a reliable region of contact for the switch. The switch is fabricated using silicon nitride as the armature structural layer and silicon dioxide as the sacrificial layer supporting the armature during fabrication. Hydrofluoric acid is used to remove the silicon dioxide layer with post-processing in a critical point dryer to increase yield.

### 20 Claims, 5 Drawing Sheets

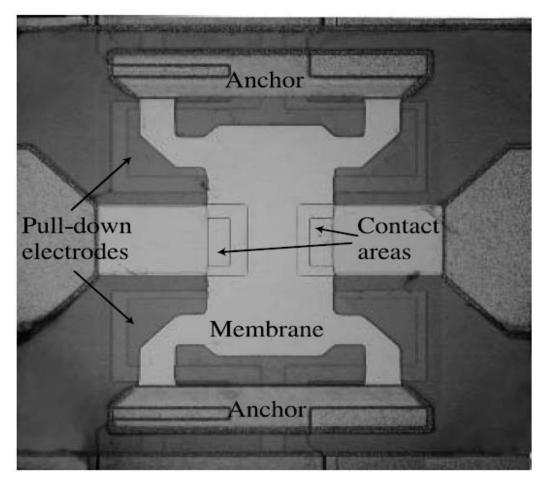


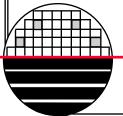
# ROCKWELL SCIENCE CENTER MEMS DC SWITCH



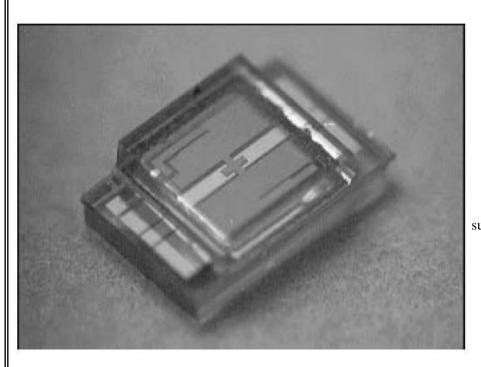


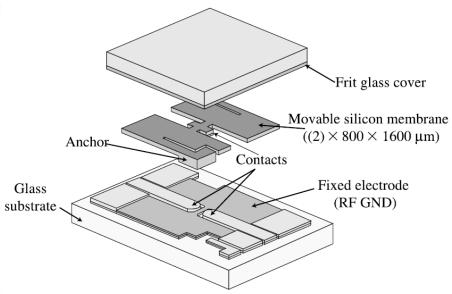
## UNIVERSITY OF MICHIGAN ALL METAL DC SWITCH

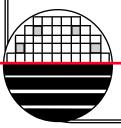




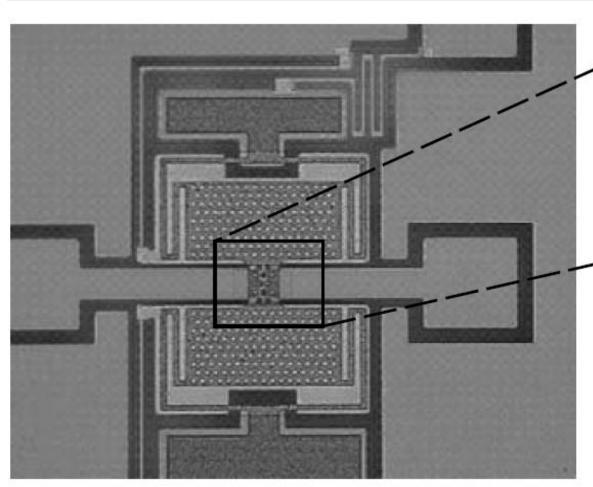
# OMRON DC CONTACT MEMS SWITCH



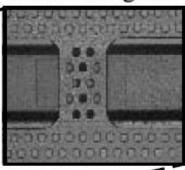




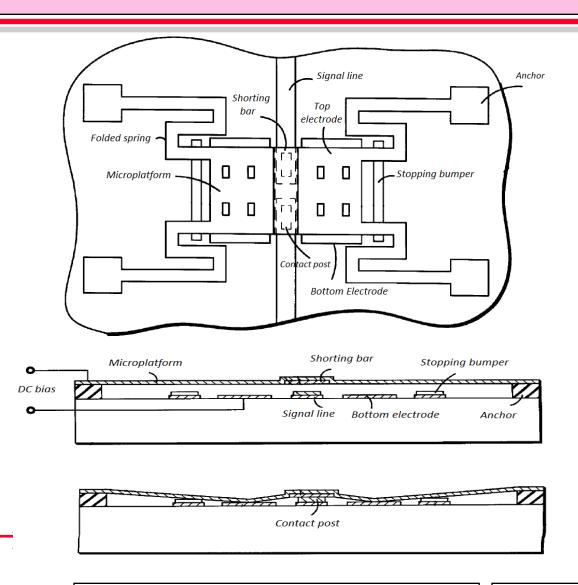
# SAMSUNG DC CONTACT SWITCH



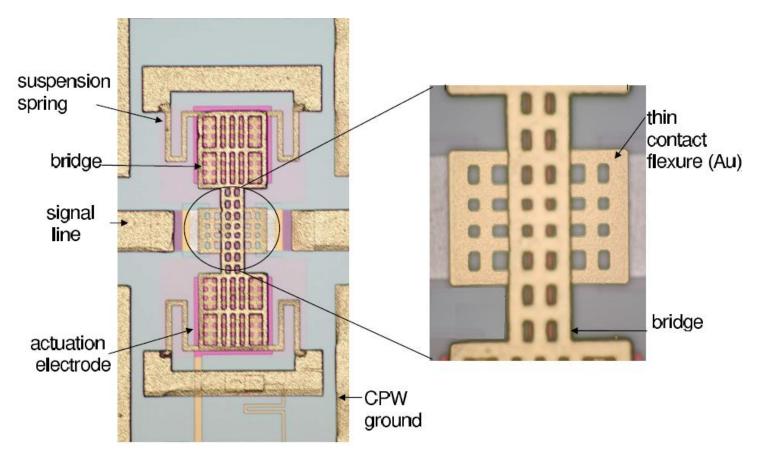
# Contact region



### MOTOROLA FOLDED SPRING DC CONTACT SWITCH



### UNIVERSITY OF TRENTO LOW ACTIVATION SWITCH

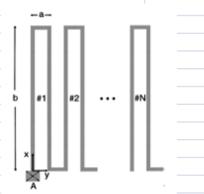


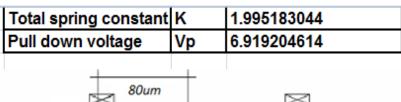


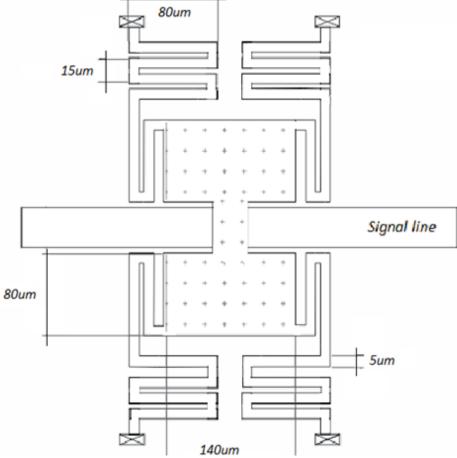
Rochester Institute of Technology

## ARTUR NIGMATULIN DESIGN

Primary length (a) 1.50E- Secondary length (b) 1.00E- Thickness (t) 2.00E-	04 06
, , ,	06
Thickness (t) 2.00E-	$\overline{}$
	06
Beam width (w) 5.00E-	
Poly (Youngs Modulus) (E) 1.60E+	11
Poly (Poissons Ratio) (v) 0.	22
Shear Modulus (G) 6.56E+	10
X-axis moment of inertia (lx) 3.33E-	24
Z-axis moment of inertia (Iz) 2.08E-	23
Polar moment of inertia (lp) 2.42E-	23
Torsion Constant J 9.98E-	24
Initial gap (g0) 2.00E-	-06
Area 1.12E-	-08
Number of meanders	4
Spring constant of 1 meander 0.49879	96
Actuation Electrodes length 1.40E-	04
Actuation Electrodes width 8.00E-	05





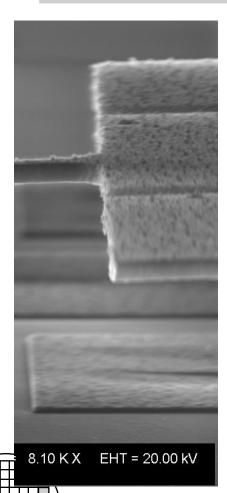


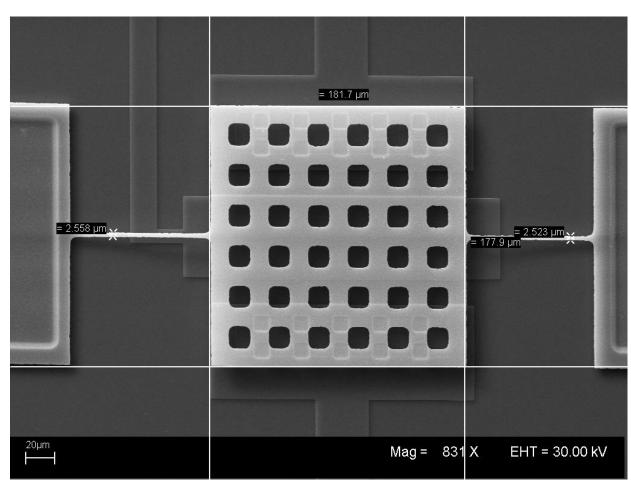


© May 17, 2012 Dr. Lynn Fuller, Professor

Page 25

## RIT SWITCHES BY ANDREW ESTROFF

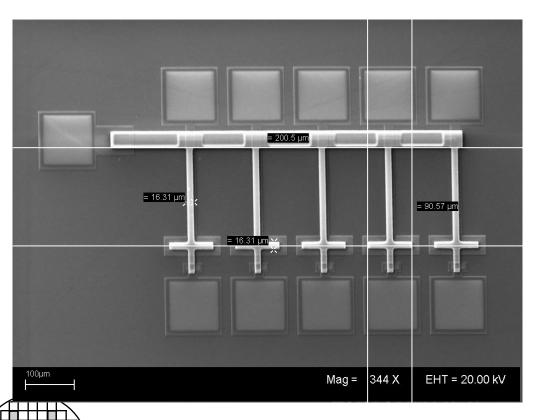


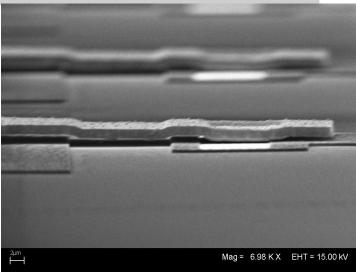


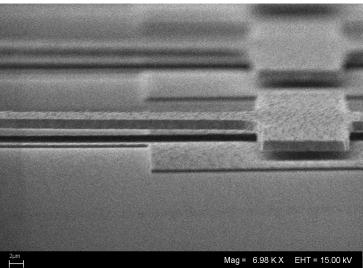
Rochester Institute of Technology Microelectronic Engineering

**Full Paper** 

# RIT MULTIPLEXER BY ANDREW ESTROFF





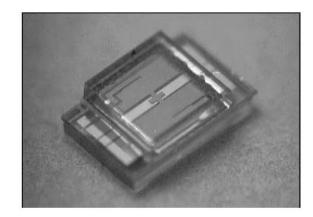


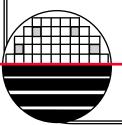
Rochester Institute of Technology

# **COMMERCIAL MEMS SWITCHES**

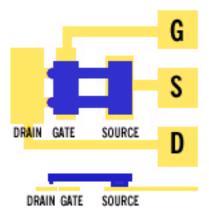


Omron Co. 2SMES-01





### **COMMERCIAL MEMS SWITCHES**

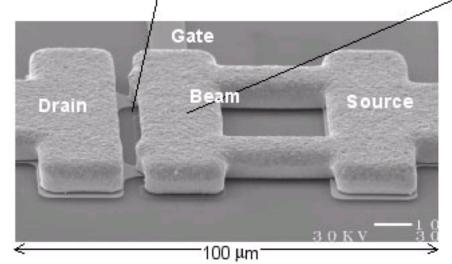


### Radant MEMS Switch (continued)

### Operation

Under the cap, the beam is deflected by applying a voltage between the gate and source electrodes. The free end of the beam contacts the drain and completes an electrical path between the drain and the source.







### RADANT MEMS RMSW200 SWITCH





### RMSW200-EV12 **Evaluation Test Board** DC to 12 GHz for RMSW200™

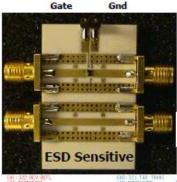
### General Description

The evaluation test board has one RMSW200™ SPST RF switch connected to two SMA RF connectors, as well as a calibration line. The board requires an external supply to provide the gate actuation voltage.

(Test Board minus Calibration Line Loss)

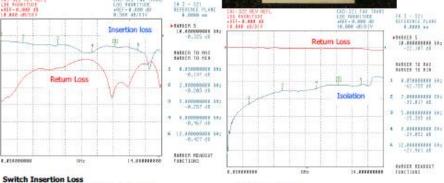
Port In/out (Drain)

Calibration Port In/out



Port In/out (Source)

Calibration Port In/out





**Test Board Insertion Loss** 

RADANT MEMS INC. Fax: 978-562-6277

+/- 90 V

0 V

Email: sales@radantmems.com Visit www.radantmems.com

Phone: 978-562-3866

ON

OFF

Rochester Institute of Technology

Switch Isolation

### **COMMERCIAL MEMS SWITCHES**



Monday, May 2, 2011

### MEMS for RF

RF MEMS Switches

Reliability Enhancements

<u>MEMS</u> <u>Packaging</u>

<u>MEMS Phase</u> Shifters

# **MEMS Packaging**

**MEMS Packaging**—In the past decades, many advances have been made in the fabrication of miniaturized mechanical structures called MEMS. Yet the application of this technology is hampered by the lack of production-worthy, MEMS-compatible packages. MEMS packages must not only protect the often-fragile mechanical structures and provide the interface to the next level in the packaging hierarchy, but they must also be fabricated in a cost effective manner to allow for affordable mass-produced circuits. Since several thousand RF switches are simultaneously fabricated on a single substrate, a cost effective packaging process should perform most of the packaging steps at a wafer level, before separation into discrete circuits.

### REFERENCES

- 1. Analog Devices Co., <a href="http://www.analog.ocm/technology/mems/umRelay/index.html">http://www.analog.ocm/technology/mems/umRelay/index.html</a>
- 2. G. Rebeiz and J.B. Muldavin, IEEE Microwave Magazine, 2(4),59,(2001)
- 3. Magnetic latching MEMs RF switches. <a href="www.magfusion.com">www.magfusion.com</a>
- 4. G. M. Rebeiz, "RF MEMS Theory, Design and Technology", 1st ed. Wiley Inter-Science, 2003
- 5. Chiung-I Lee, Chih-Hsiang Ko, and Tsun-Che Huang," Design of Multi-actuation RF MEMS Switch Using CMOS Process", IEEE, 2008
- 6. Gabriel M. Rebeiz, Jeremy B. Muldavin, "RF MEMS switches and Switch Circuits",IEEE Microwave Magazine, December 2001
- 7. Kamal Jit Rangra, "Electrostatic Low Actuation Voltage RF MEMS Switches for Telecommunications", Ph.D thesis, Information and Communication Technologies, DIT-University of Trento, Italy, February 2005
- 8. L. E. Larson, R. H. Hackett, M. A. Melendes, and R. F. Lohr, "Micromachined microwave actuator (MIMAC) technology—a new tuning approach for microwave integrated circuits", IEEE Microwave and Millimeter-Wave Monolithic Circuits Symposium Digest, Boston, MA, June 1991, pp. 27–30
- 9. J. J. Yao and M. F. Chang, "A surface micromachined miniature switch for telecommunications applications with signal frequencies from DC up to 4 GHz", Rockwell Science Center, IEEE, 1995
- 10. Gabriel M. Rebeiz, "RF MEMS Switches: Status of the technology", The 12th International Conference on Solid State Sensors, Actuators and Microsystems, Boston, June 8-12, 2003



Rochester Institute of Technology

### REFERENCES

- 11. G. L. Tan, "High Performance RF MEMS Circuits and Phase Shifters", Ph.D. thesis, University of Michigan, Ann Arbor, MI, 2002
- 12. M. Sakata, Y. Komura, T. Seki, K. Kobayashi, K. Sano, and S. Horike, "Micromachined relay which utilizes single crystal silicon electrostatic actuator", 12th IEEE International Conference on Microelectromechanical Systems, pp. 21–24, 1999
- 13. Xi-Qing, "Folded spring based micro electromechanical MEM RF switch", United States Patent Number 6307452B1, October 2001
- 14. Dimitrios Peroulis, "Electromechanical Considerations in Developing Low-Voltage RF MEMS Switches", IEEE Transactions on microwave theory and techniques, Vol.51, No. 1, January 2003
- 15. Jérémie Bouchaud, Director and Principal Analyst, MEMS & Sensors, <u>iSuppli</u>, "RF MEMS switches and varactors finally arrive", MEMS Investor Journal, October 2010
- 16. R. J. Roark and W. C. Young, Formulas for Stress and Strain, 6th edition, McGraw-Hill, New York, 1989
- 17. J. M. Gere and S. P. Timoshenko, Mechanics of Materials, 4th edition, PWS Publishing Company, Boston, 1997
- 18. V. L. Rabinov, R. J. Gupta and S. D. Senturia, "The effect of release etch holes on the electromechanical behavior of MEMS structures", International Conference on Solid-State Sensors Actuators, Chicago, IL, June 1997, pp. 1125-1128
- 19. G. K. Fedder, "Simulation of Microelectromechanical systems", Ph.D. thesis, Electrical Engineering and Computer Science, University of California at Berkeley, USA, 1994
- 20. Stephen D. Senturia, "Microsystem Design", 1st ed. Boston-Dordrecht-London: Kluwer Academic Publishers, 2002

### HOMEWORK – MEMS SWITCHES

1. Design a process to make a MEMS switch at RIT.

Or

2. Find out who sells mems switches and get some information on their products including price.

Or

3. Find a recent technical paper on MEMs switches. Summarize it on one page and attach a copy of the full paper.

