ROCHESTER INSTITUTE OF TEHNOLOGY MICROELECTRONIC ENGINEERING

# MEMS Capacitor Sensors and Signal Conditioning

Dr. Lynn Fuller

Dr. FullersWebpage: <u>http://people.rit.edu/lffeee</u> Electrical and Microelectronic Engineering Rochester Institute of Technology 82 Lomb Memorial Drive Rochester, NY 14623-5604 Email: <u>Lynn.Fuller@rit.edu</u> ProgramWwebpage: <u>http://www.microe.rit.edu</u>

Rochester Institute of Technology Microelectronic Engineering - 4-2-11 capacitor\_sensors.ppt

© April 2, 2011 Dr. Lynn Fuller, Professor

### **OUTLINE**

Capacitors Capacitors as Sensors Chemicapacitor Diaphragm Pressure Sensor Condenser Microphone Capacitors as Electrostatic Actuators Signal Conditioning References Homework

**Rochester Institute of Technology** 

Microelectronic Engineering

© April 2, 2011 Dr. Lynn Fuller, Professor







### **DIELECTRIC CONSTANT OF SELECTED MATERIALS**

Vacuum	1	Methanol	30 3		
Air	1.00059	Photoresist			
Acetone	20	Plexiglass	3.4		
Barium strontium	500	Polyimide	2.8		
titanate		Rubber	3		
Benzene	2.284	Silicon	11 7		
Conjugated	6 to 100.000		11.7		
Polymers		Silicon dioxide	3.9		
Ethanol	24.3	Silicon Nitride	7.5		
Glycerin	42.5	Teflon	2.1 80-88		
Glass	5-10	Water			

http://www.asiinstruments.com/technical/Dielectric%20Constants.htm

© April 2, 2011 Dr. Lynn Fuller, Professor

### **CALCULATIONS**

the second se										
	A	В	С	D	E	F	G	Н	I	
1	Rochester	r Institute o	of Technol	ogy					8-Apr-08	
2	Dr. Lynn Fuller Microelectronic Engin				eering, 82 Lomb Memorial Dr., Rochester, NY 14623					
3										
4	To use this spread sheet enter values in the white boxes. The rest of the sheet is protected and should not									
5	changed u	nless you a	ire sure of t	he consequ	ences. The results are displayed in the purple boxes.					
6										
7	Capacitance of Two Parallel Plates									
8 Capacitance = eoer Area			Area/d			C =	8.85E-12	F		
9				eo = Pe	ermitivitty of	free space	8.85E-14	F/cm		
10				er = relative permitivitty =			1			
11						Area =	1.00E-02	cm2		
12				number	of pairs of p	olates, N =	1			
13				distanc	e between p	olates, d =	1	μm		
14				lf rou	nd plates, D	lates, Diameter =	0	μm		
15				If rectangular plates, length =			1000	μm		
16				If rectangular plates, width =			1000	μm		
17	Force Bet	ween Two	Parallel F	Plates		Force =	4.43E-04	N		
18	Electrosta	Electrostatic Force= eoer Area V <sup>2</sup> /2d <sup>2</sup>			Applied Voltage, V =		10	volts		
19										
20	Capacitar	nce for ver	y Thick Int	erdigitated	d Fingers					
21		C = (N-1) e	eoer L'h/s		Capac	itance, C =	1.77E-13	F		
22				N	lumber of F	ingers, N =	101			
	7	Microelectro	oni <del>c Engineerii</del>	ıg						
Ź			Ô	Anril 2, 2011	Dr. Lynn Fulle	er. Professor			]	
	Sapin 2, 2011 Di. Lynn Funci, 11005501 Page 6									









Solution: let b = 5 mm, a = 0.2mm, plastic er = 3 the equation above gives C/L = 51.8 pF/m C = 51.8 pF



## 

One plate moves relative to other changing gap (d)

Center plate moves relative to the two fixed plates





Rochester Institute of Technology

Microelectronic Engineering

© April 2, 2011 Dr. Lynn Fuller, Professor



### **CHEMICAL SENSOR**

Two conductors separated by a material that changes its dielectric constant as it selectively absorbs one or more chemicals. Some humidity sensors are made using a polymer layer as a dielectric material.



**Change in Dielectric Constant (er)** 





### DIAPHRAGM WITH CAPTURED VOLUME



© April 2, 2011 Dr. Lynn Fuller, Professor

### **CONDENSER MICROPHONE**







© April 2, 2011 Dr. Lynn Fuller, Professor

### DELTA CAPACITANCE TO AC VOLTAGE



If Cx is fixed Vo is zero. If Cx changes there will be a change in current and a corresponding change in Vo

Example: Let Vin = 3 volts, C = 10 pF, microphone action causes C to change by 0.1pF at 1000 Hz. Calculate the output voltage.



Microelectronic Engineering

© April 2, 2011 Dr. Lynn Fuller, Professor





### **SC EXAMPLE**

- 1. The sampling frequency fs must be much higher than the signal frequencies
- 2. The voltages at node 1 and 2 must be unaffected by switch closures.
- 3. The switches are ideal.
- 4. S1 and S2 are not both on at same time. (use non overlapping clocks)



**Example:** for audio applications with frequencies up to 10KHz, we select switch frequency of 500KHz, for a 1 MEG ohm resistor we find that

#### C = 1/(500K 1MEG) = 2 p/F

































### SIMILAR IDEA FOR WIRELESS TEMPERATURE



### Network Analyzer

Rochester Institute of Technology Microelectronic Engineering



© April 2, 2011 Dr. Lynn Fuller, Professor











© April 2, 2011 Dr. Lynn Fuller, Professor



#### **MEMS Capacitor Sensors VERSION 1 OP AMP** Op Amp Frequency Response OP Amp Con: SMU1 Val: 6.0000 V Swp: SMU3 Start: -1.5000 \ Stop: -0.5000 \ Step: 1.0000m ٧O 4 Pts: 1001 Con: SMU2 Val: -6.0000 \ 20 Con: SMU4 177) <del>I</del> Val: 0.0000 A 0 VN Hind of Fit#2 Cursors: X -1.1720 -1.0640 -20 Non -1.1730 3.4750 p:-4.5393K 0\*\*\* 100000 10000000 nt:-5.32121 .*4*0 Frequency Hz OPAI Gain ~5000 Offset 1.17 mV GBW = 500 KHzRochester Institute of Technology Microelectronic Engineering © April 2, 2011 Dr. Lynn Fuller, Professor Page 46

### **BASIC TWO STAGE OPERATIONAL AMPLIFIER**



### **SPICE ANALYSIS OF OP AMP VERSION 2**

.incl rit\_sub\_param.txt

- m1 8 9 7 6 cmosn w=9u l=5u nrd=1 nrs=1 ad=45p pd=28u as=45p ps=28u
- m2 1 10 7 6 cmosn w=9u l=5u nrd=1 nrs=1 ad=45p pd=28u as=45p ps=28u m3 8 8 4 4 cmosp w=21u l=5u nrd=1 nrs=1 ad=102p pd=50u as=102p
- ps=50um4 1 8 4 4 cmosp w=21u l=5u nrd=1 nrs=1 ad=102p pd=50u as
- m4 1 8 4 4 cmosp w=21u l=5u nrd=1 nrs=1 ad=102p pd=50u as=102p ps=50u
- m5 7 5 6 6 cmosn w=40u l=5u nrd=1 nrs=1 ad=205p pd=90u as=205p ps=90u
- m6 2 1 4 4 cmosp w=190u l=5u nrd=1 nrs=1 ad=950p pd=400u as=950p ps=400u
- m7 2 5 6 6 cmosn w=190u l=5u nrd=1 nrs=1 ad=950p pd=400u as=950p ps=400u
- m8 5 5 6 6 cmosn w=40u l=5u nrd=1 nrs=1 ad=205p pd=90u as=205p

vdd 4 0 3 vss 6 0 - 3

VSS 0 U - 3

- cprobe 2 0 30p Rprobe 2 0 1 meg
- cc 1 2 0.6p
- mr1 20 20 4 4 cmosp w=6u l=10u nrd=1 nrs=1 ad=200p pd=60u as=200p ps=60u
- mr2 5 5 20 4 cmosp w=6u l=10u nrd=1 nrs=1 ad=200p pd=60u as=200p ps=60u

\*\*\*\*\*

Rochester Institute of Technology

Microelectronic Engineering

© April 2, 2011 Dr. Lynn Fuller, Professor

Page 48



\*\*\*dc open loop gain\*\*\*\*\*\*\* vi1 9 0 0 vi2 10 0 0 \*.dc vi2 -0.002 0.002 1u .dc vi2 -1 1 0.1m \*\*\*\*\*open loop frequency characteristics\*\*\*\*\* \*vi1 9 0 0 \*vi2 10 0 dc 0 ac 1u \*.ac dec 100 10 1g .end





For current flowing to the right (ie V1>V2) the PMOS transistor will be on if V1 is greater than the threshold voltage, the NMOS transistor will be on if V2 is <4 volts. If we are charging up a capacitor load at node 2 to 5 volts, initially current will flow through NMOS and PMOS but once V2 gets above 4 volts the NMOS will be off. If we are trying to charge up V2 to V1 = +1 volt the PMOS will never be on. A complementary situation occurs for current flow to the left. Single transistor switches can be used if we are sure the Vgs will be more than the threshold voltage for the specific circuit application. (or use larger voltages on the gates)











## TWO PHASE NON OVERLAPPING CLOCK

**MEMS** Capacitor Sensors







